

Charge-optimal control of battery-powered equipment

Application to FMTC badminton robot

Outline

1. Introduction
2. Modeling
3. Charge-optimal control



Outline



1. Introduction

1. General context
2. Presentation of the badminton robot

2. Modeling

3. Charge-optimal control

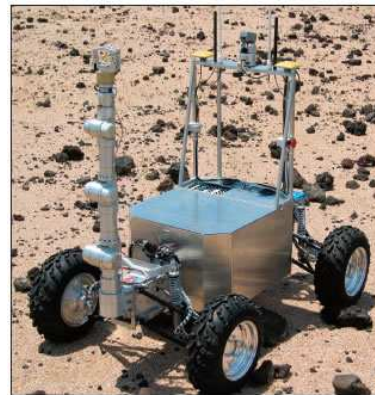


General context

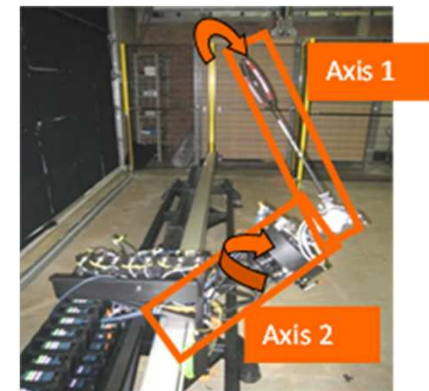
- + There is growing interests in electrification of drive trains
- + Battery technology plays significant role



Daimler electrical car charging



Nasa's four-wheeled autonomous mobile robot for lunar and Mars missions



FMTC badminton robot arm

- + However, batteries are characterized by limited energy storage capacity → this limits autonomy



How can the battery usage be extended?

+ Two possible levers:

- Battery technology: use battery with high energy density
- Control strategy: optimize battery capacity utilization
 - Eco-driving mode: driver is helped to achieve a higher battery utilization by reducing driving aggressiveness
 - Similar methodology can be applied for industrial applications

+ GOAL:

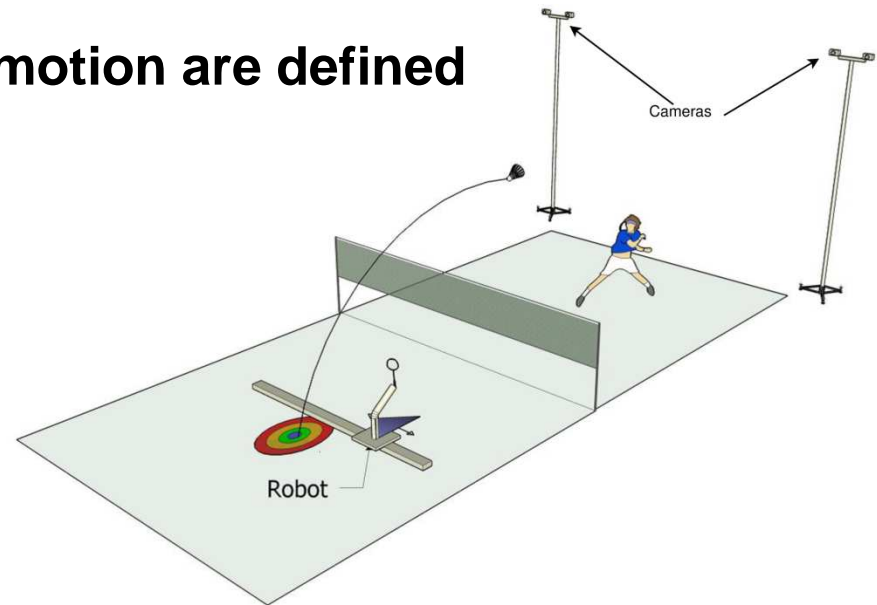
- charge-optimal control for the badminton robot arm

→ Set control parameters so that the utilized charge is minimal

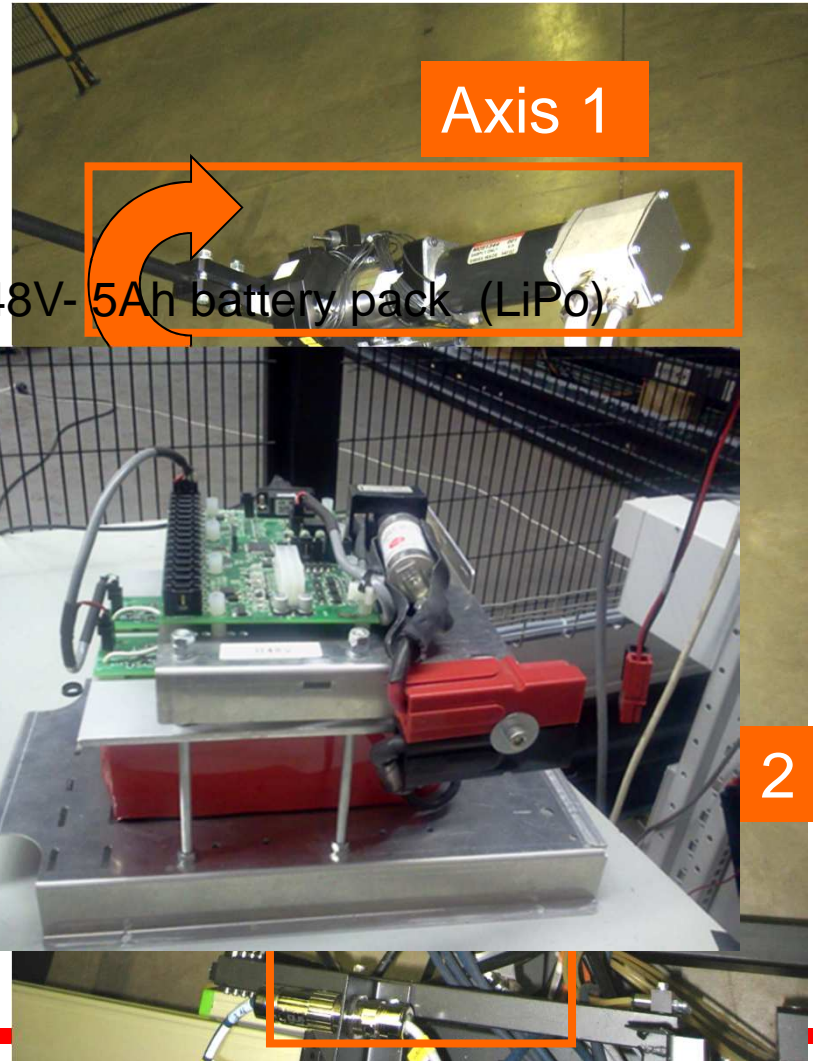
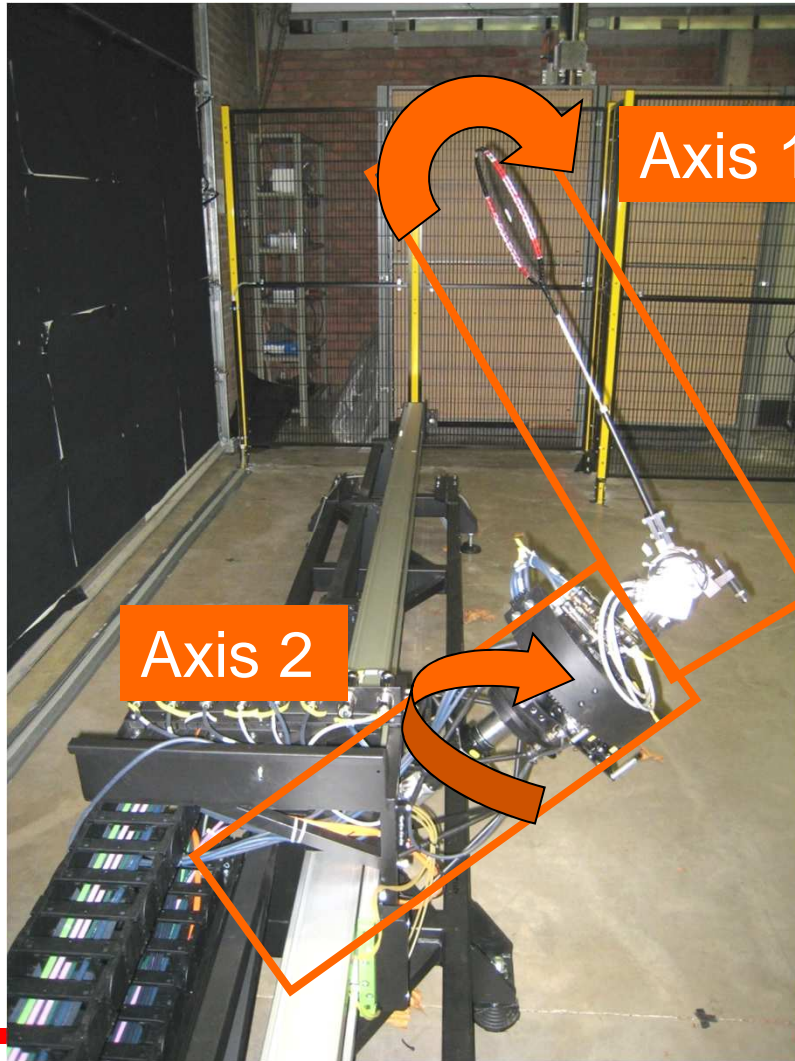


FMTC – Badminton robot

- + 3 axis robot: linear, arm rotation and hit
- + Camera images of the shuttle and calculation of its estimated trajectory allow the interception point to be determined
- + Target parameters of the arm motion are defined
 - Distance to be travelled: θ
 - Maximum velocity: V_{\max}
 - Maximum acceleration: A_{\max}



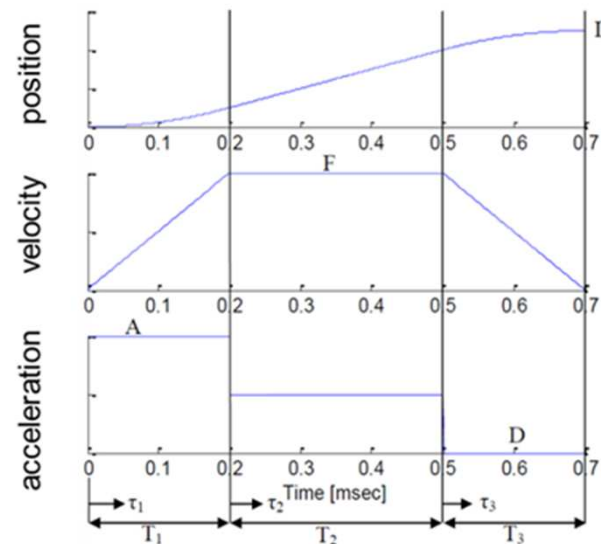
FMTC – Badminton robot



The current control strategy

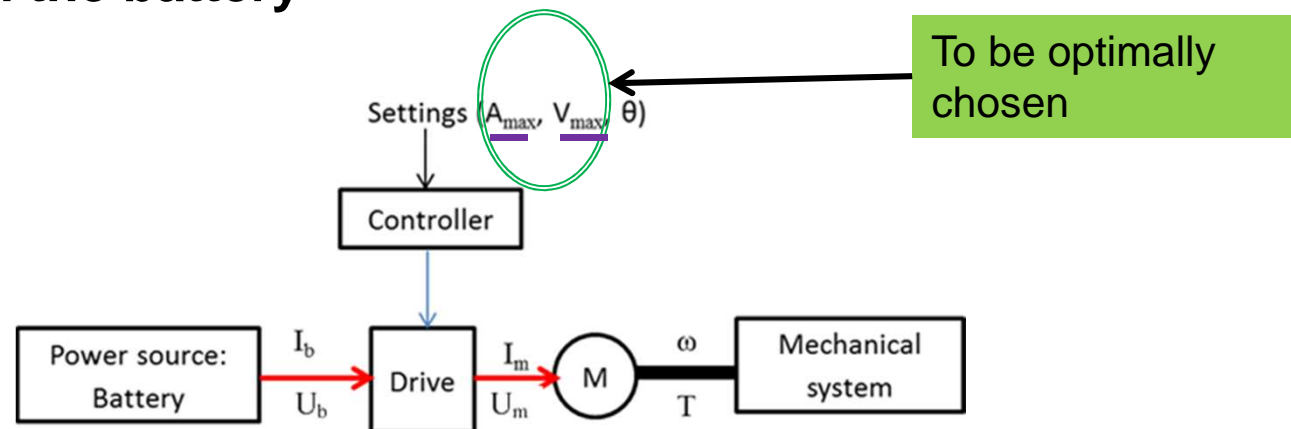
+ Time optimal:

- The arm moves as fast as possible to intercept the shuttle
- This leads to high velocity and high acceleration
- Also high currents are drawn from the battery → the battery usage time is reduced



Alternative control strategy?

- + FMTC has developed and applied “Energy-optimal” on the linear motion control which allows almost 60% of energy savings
- + For the arm motion, the optimization will concern the charge drawn from the battery



Outline

1. Introduction

2. Modeling

1. Power prediction model
2. Battery response model

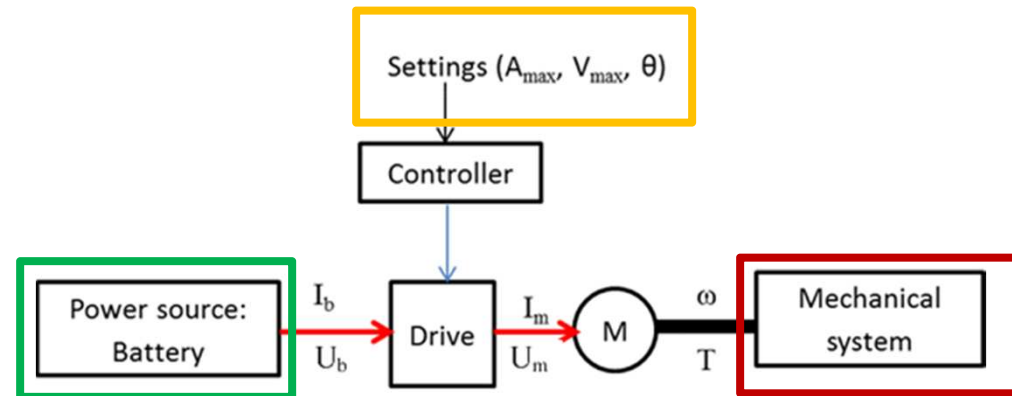
3. Charge-optimal control



Battery and mechanical system modeling for designing the optimal controller

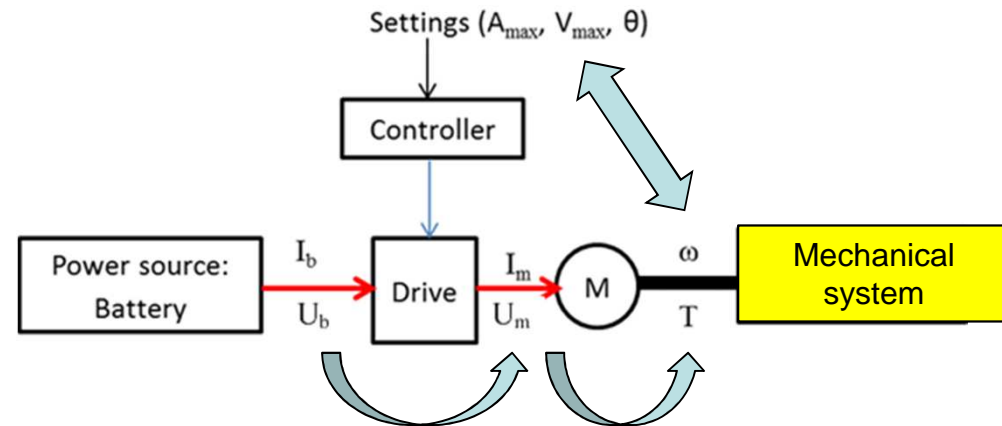
+ Two models are built:

- Power predictor to establish the relationship between the control settings (A_{max} , V_{max} , θ) and the electrical measured power
- Battery equivalent circuit model: to predict the battery response to given control settings



Power prediction model

- + Power balance between the electrical and the mechanical part of the system



$$P_e - L_e = P_m + L_m + P_s$$

Electrical power Electrical losses Mechanical power Mechanical losses Idle power



Power prediction model

- + **Power balance between the electrical and the mechanical part of the system**

$$P_e - L_e = P_m + L_m + P_s$$

$$P_e = U_b I_b \quad \text{electrical power from the battery}$$

$$L_e = K_b I_b^2 + K_m I_m^2 \quad \text{ohmic losses in line before and after the drive}$$

$$P_m = T_m \omega = J \alpha \omega \quad \text{mechanical power at the arm}$$

$$L_m = \text{sign}(\omega) \omega T_f + C \omega^2 \quad \text{mechanical losses due to dry and viscous friction}$$

P_s is the idle power necessary for holding the robot arm in a given position

$$I_b = K_i U_m I_m \quad K_i \text{ is dependent on the battery state of charge (SoC)}$$



Power prediction model

- + For dynamic motions the motor is approximately proportional to the acceleration and the velocity to the voltage
- + The power equation becomes

$$P = U_b I_b \equiv J\alpha\omega + \text{sign}(\omega)\omega T_f + K_1(\text{SoC})\alpha^2\omega^2 + K_2(\text{SoC})\alpha^2 + P_{idle}$$

- + This result in parameter estimation problem:

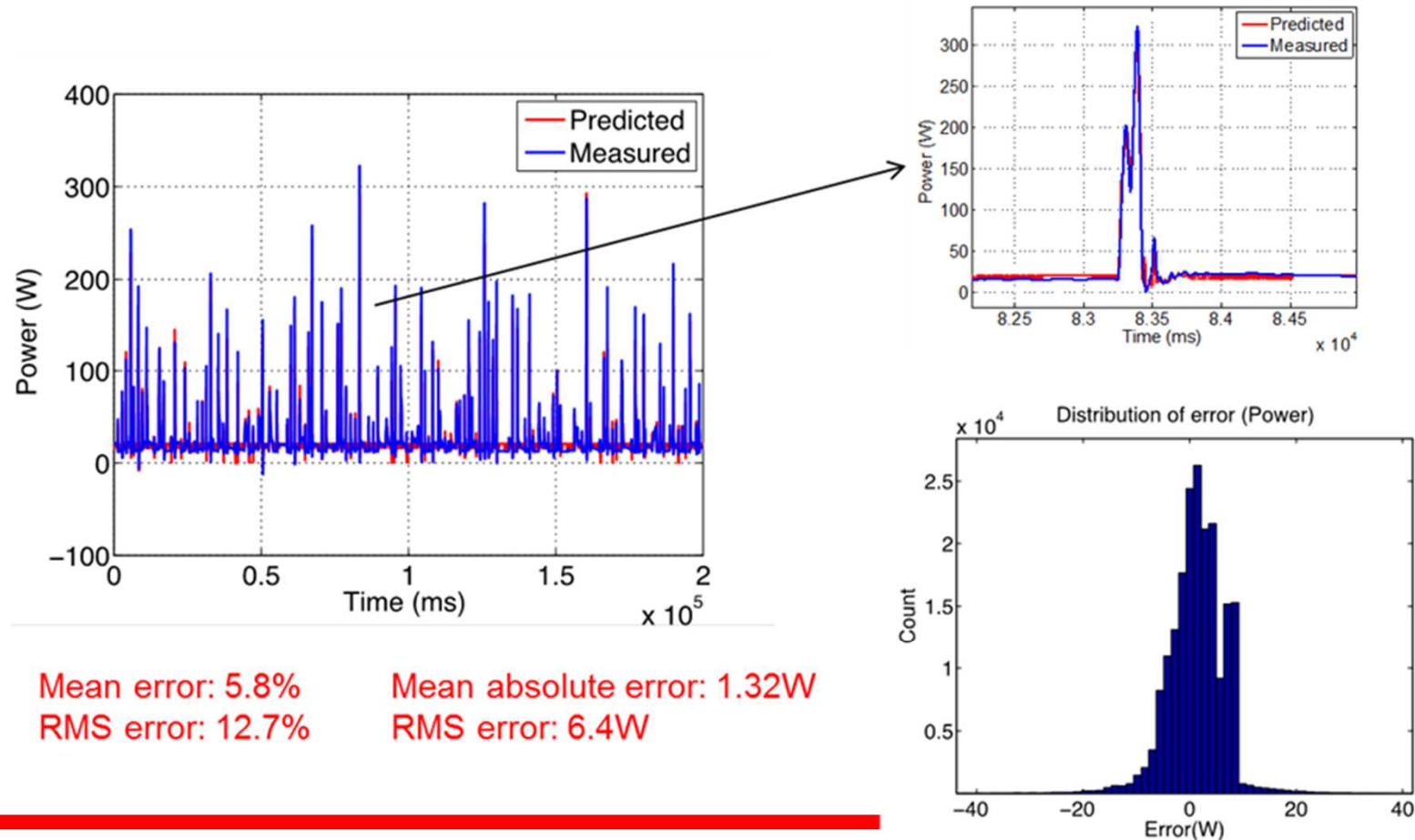
- To be estimated: $J, T_f, K_1, K_2, P_{idle}$
- Measured or known form settings: α, ω, U_b, I_b

Parameter estimation using least squared method



Power model validation

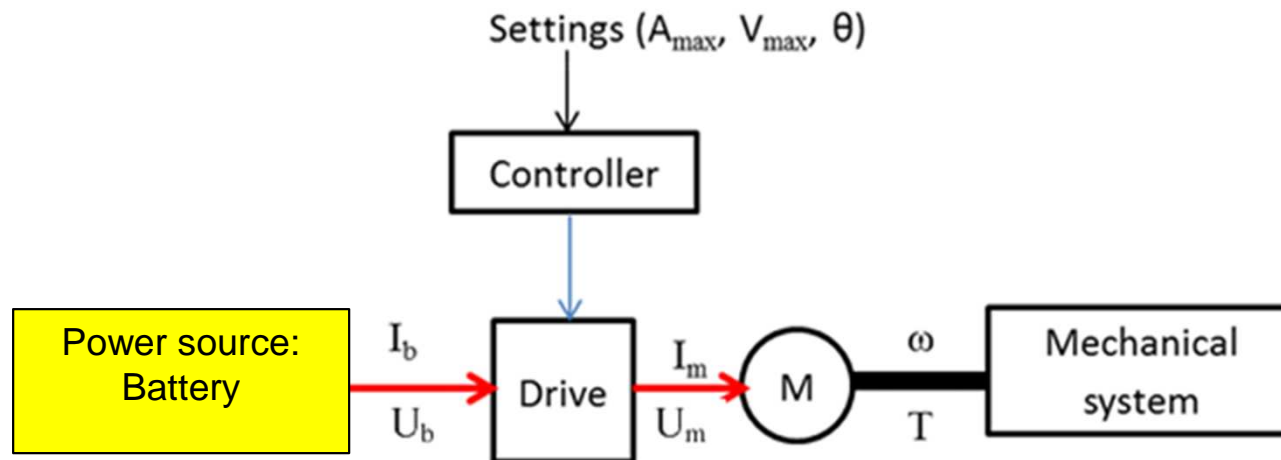
+ The model is validated using validation dataset



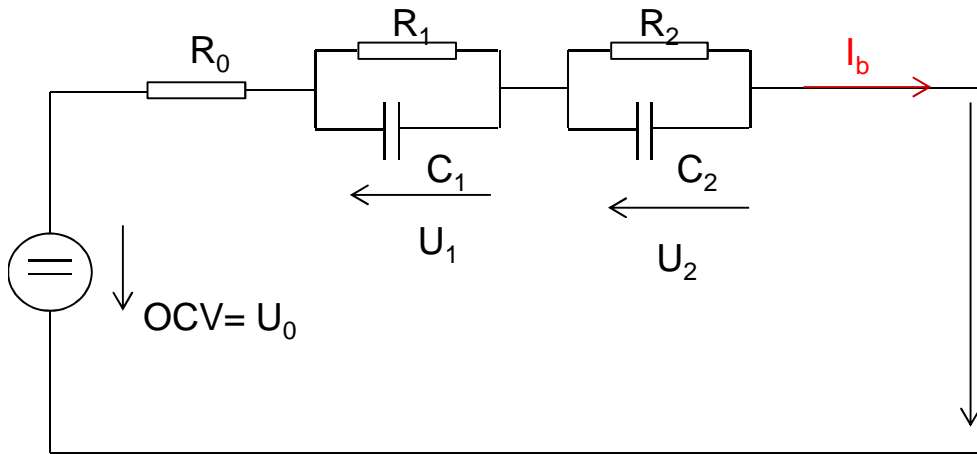
Battery modeling

+ Two models are built:

- Power predictor to establish the relationship between the control settings (A_{\max} , V_{\max} , θ) and the electrical measured power
- Battery equivalent circuit model: to predict the battery response to given control settings



Battery Equivalent Circuit Model



$$U_b(t) = OCV - R_0 I_b - \sum_{k=1}^2 R_k I_k$$

U_b

$$\tau_k = R_k C_k$$

$$U_1 = R_1 I_1$$

$$U_2 = R_2 I_2$$

2 RC pairs are enough to capture the dynamic behavior of the battery

Parameters to estimate:
OCV; R_0 ; R_1 ; C_1 ; R_2 ; C_2 as a function of soc

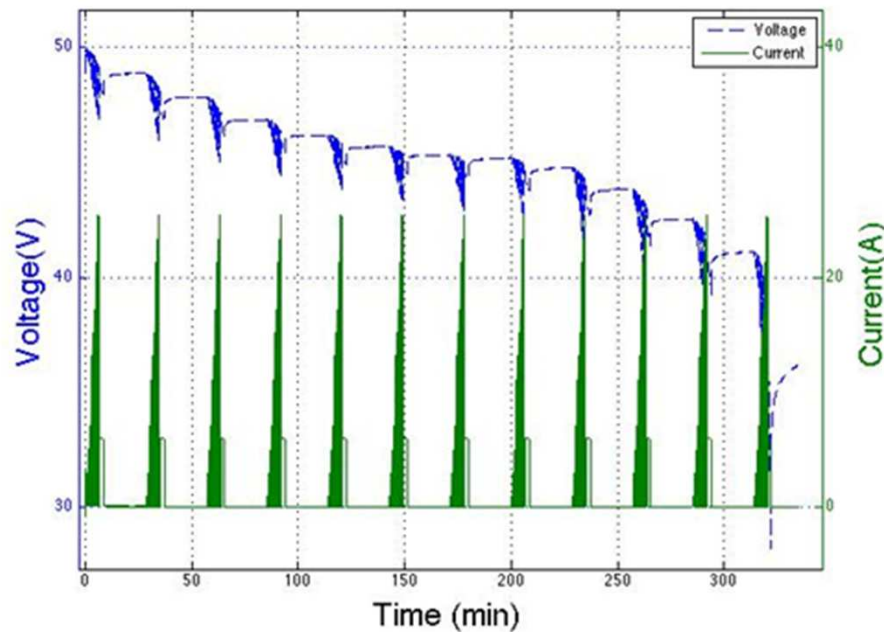


Least squared method is used



Parameters estimation

- + **Experimental HPPC (Hybrid Pulse Power Characterization) data are used for parameters estimation**

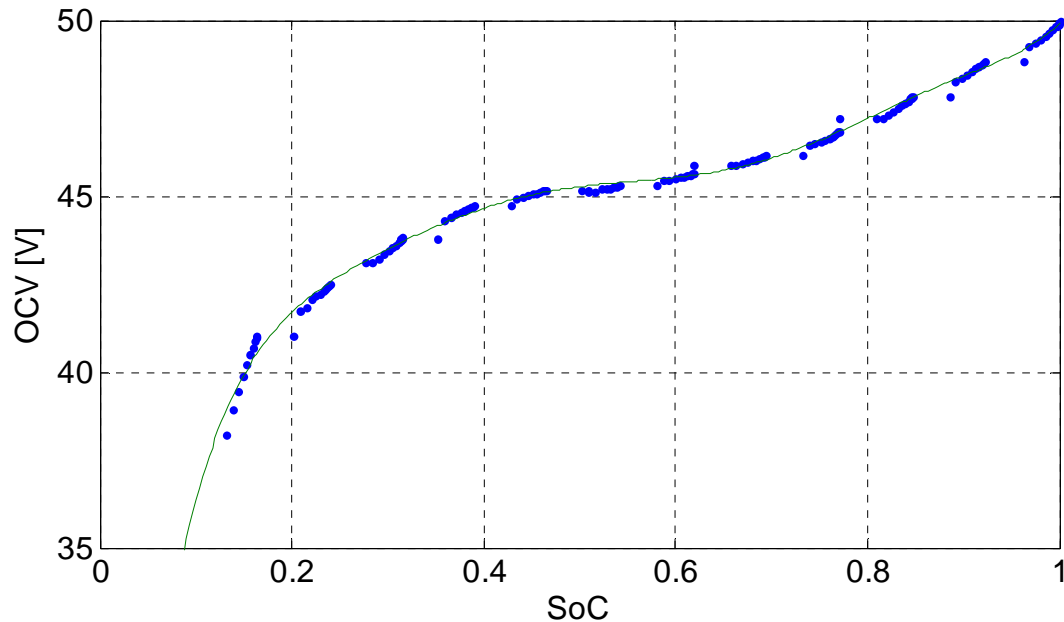


- The parameters are estimated for different SoC values
- Curves can be fitted giving these parameters i.f.o. SoC



Parameters estimation

- + **OCV=f(SoC): a polynomial or an exponential function to be used in the model can be fitted**



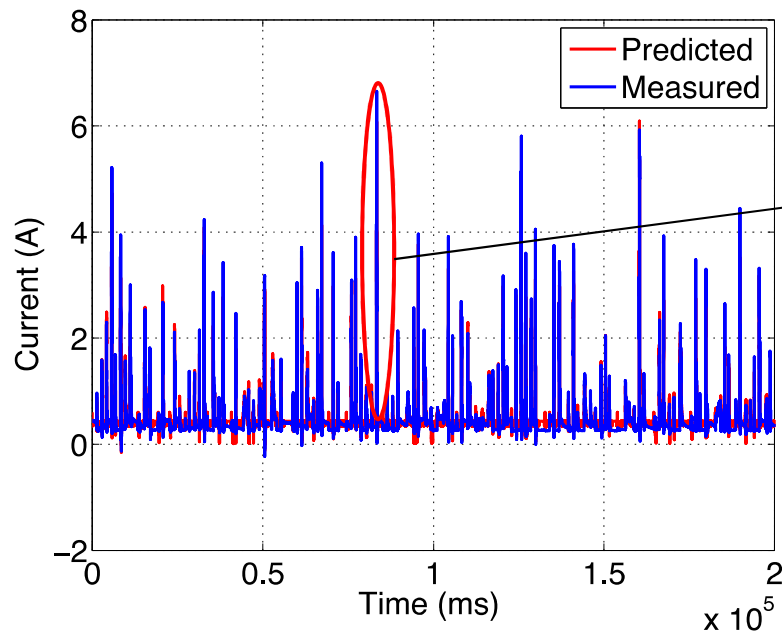
The other parameters are estimated in the same way

Estimated parameters are used in the battery model to calculate the voltage response

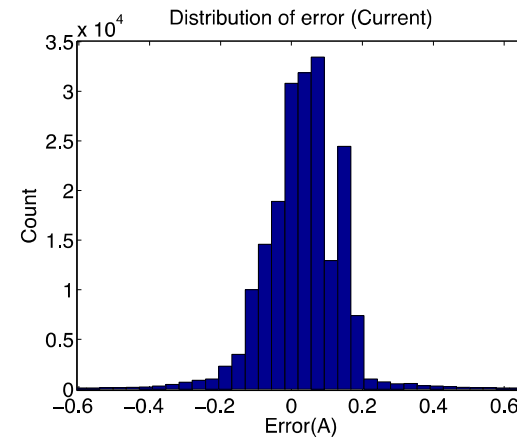
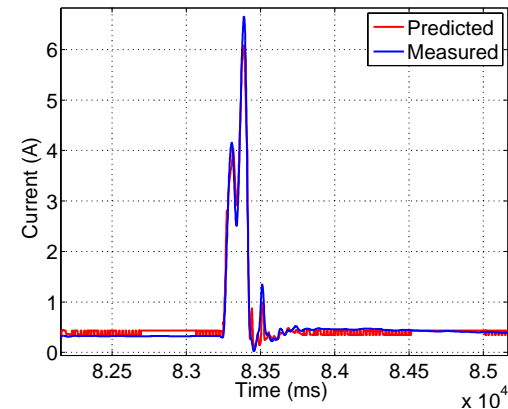


Model validation: current prediction

+ Current prediction results

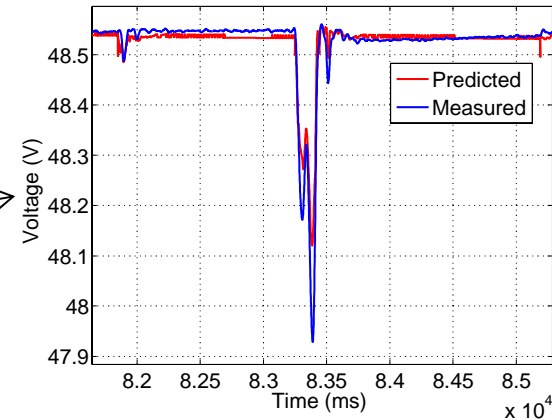
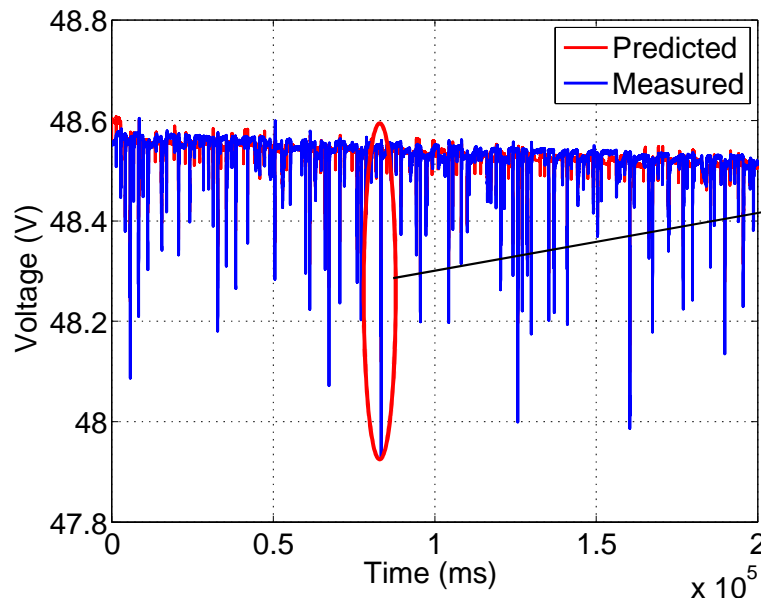


Mean absolute error: 0.032A
RMS error: 0.13A

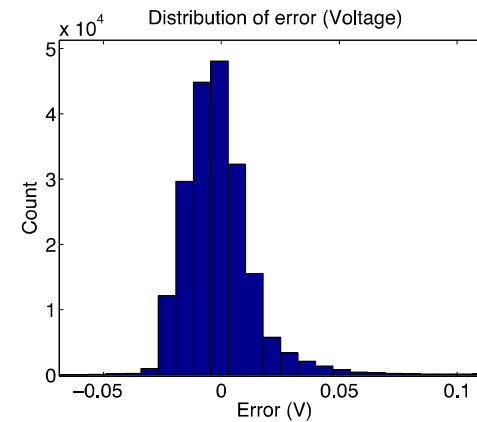


Model validation: voltage prediction

+ Voltage prediction with actual position



Mean absolute error: 0.00072V
RMS error: 0.017V



Outline

1. Introduction

2. Modeling

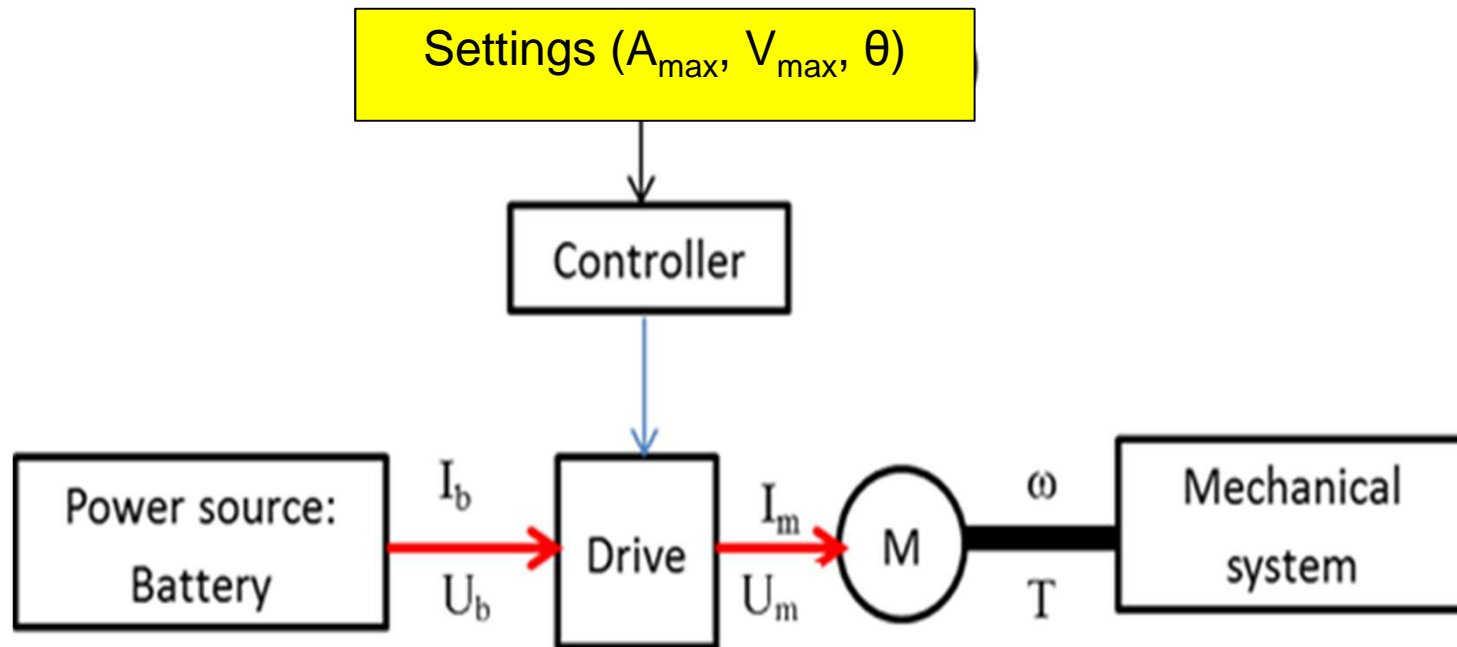
3. Charge-optimal control

1. Optimization problem formulation
2. Design of the controller
3. Comparison with other control strategies



Control optimization

- + Chose optimally the control settings
- + The power model and the battery model are used to design the control strategy that minimizes charge utilization



Design of the optimized control: problem formulation

Given a desired angular distance to travel, find the control variable A_{\max} and V_{\max} so that:

- the charge drawn from the battery is minimal between the departing point θ_1 and the arrival point θ_2 of the movement.

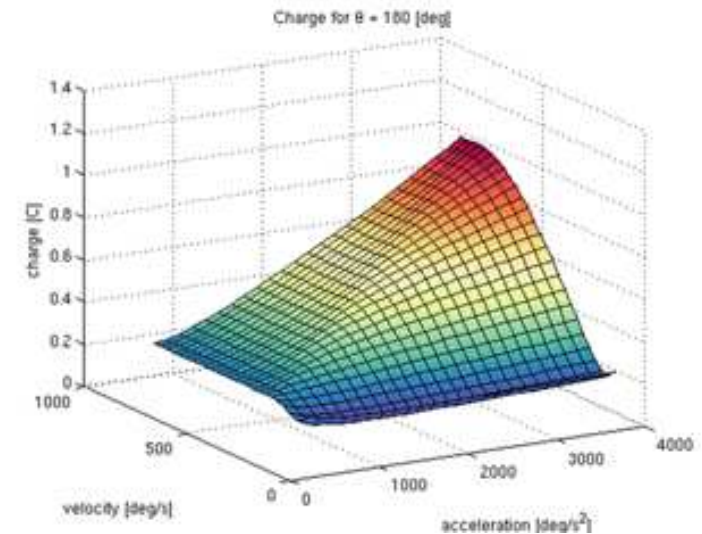
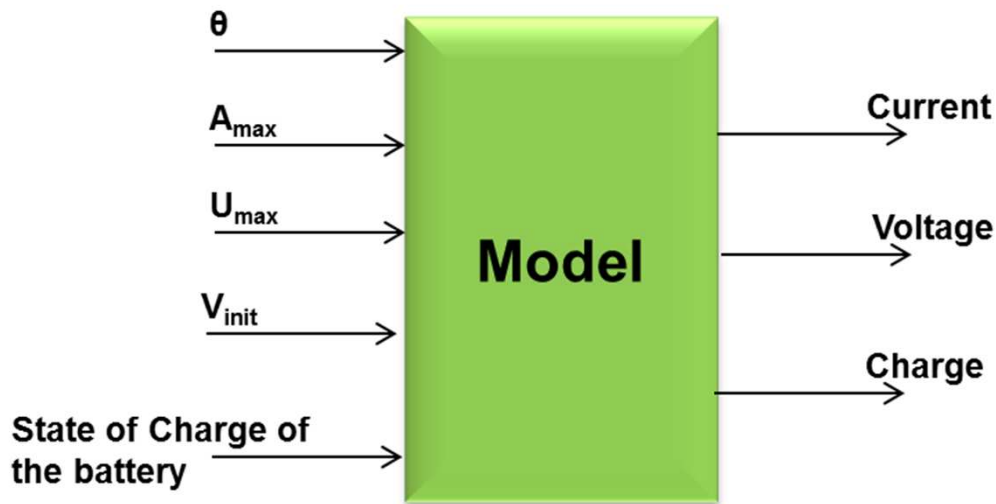
Subject to the following constraints:

- $T < T_{\max}$ (max travel time)
- $V > 35V$
- $I < 100 A$



Function to minimize: Utilized charge

- + The integrated model is simulated to evaluate the utilized charge



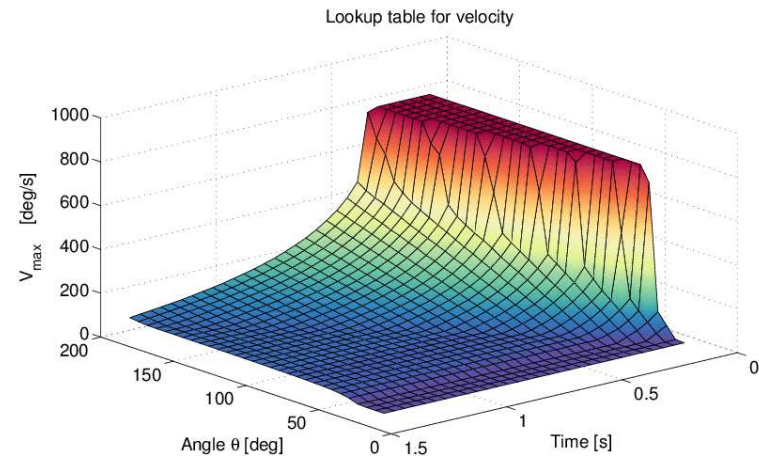
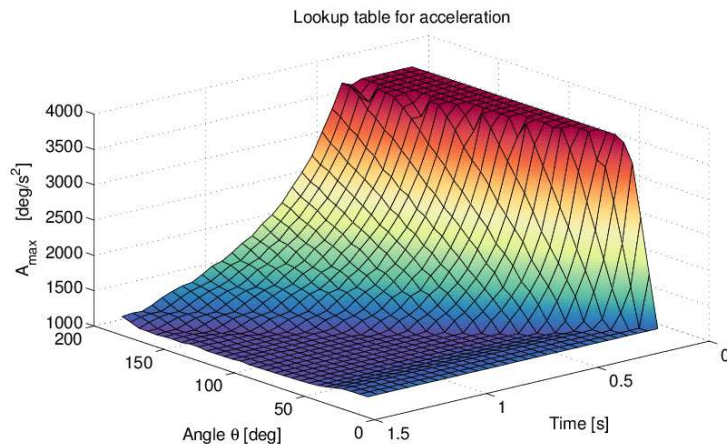
- + For each combination (θ , Initial Voltage, Travel time) the settings (A_{max} , V_{max}) minimizing the charge are calculated



The optimization solution

- + The optimized solution (A_{max_opt} , V_{max_opt}) leading to minimal charge is obtained by constrained gradient optimization
- + The results are stored in look-up tables giving

$$A_{max_opt} = f_A(T, \theta, V_{init}) \text{ and } V_{max_opt} = f_V(T, \theta, V_{init})$$



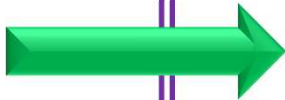
Outline

1. Introduction

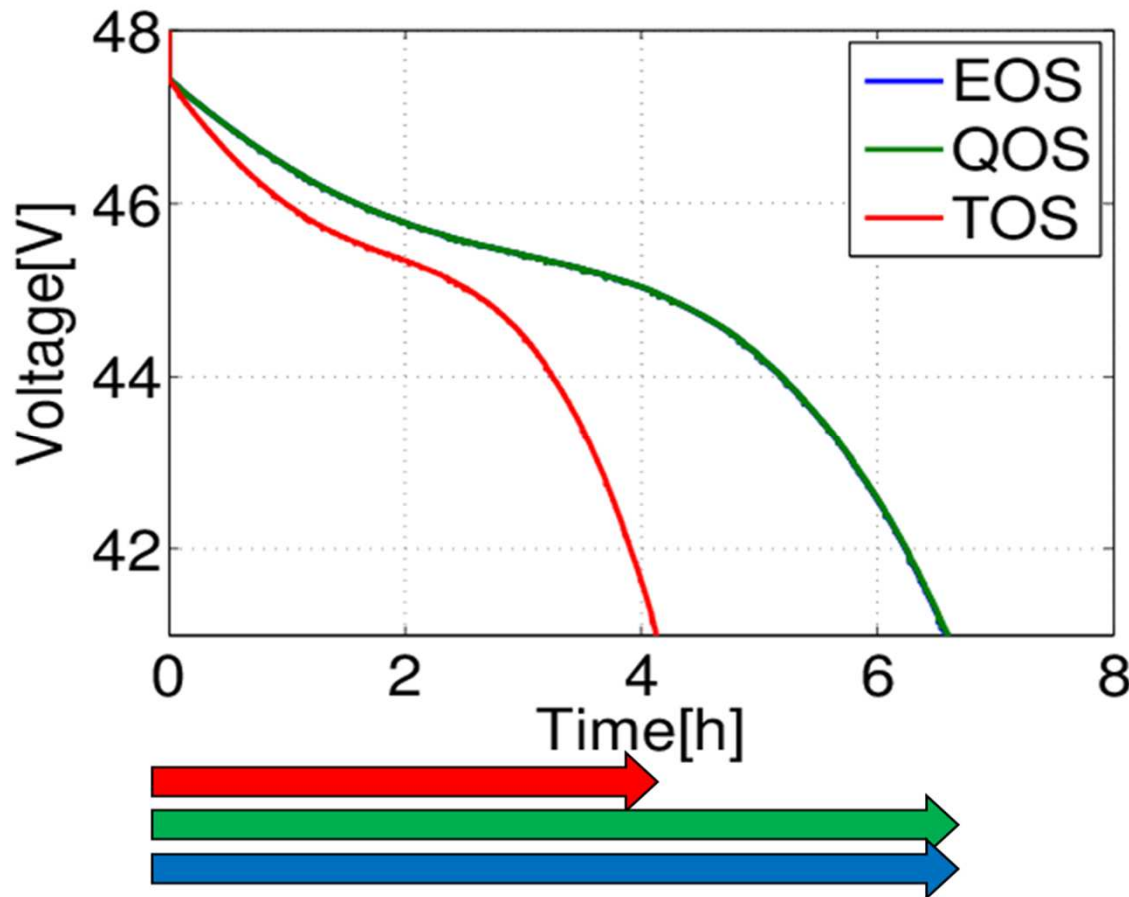
2. Modeling

3. Charge-optimal control

1. Optimization problem formulation
2. Design of the controller
3. Comparison with other control strategies



The optimized controller allows to longer use the battery



- + A sequence of robot motions is used to discharge the battery from 48V to 40V
- + 3 different control strategies are compared
- + QOS allows using longer the battery



Conclusion

- + **Charge-optimal control allows to longer use batteries**
- + **Charge-optimal is equivalent to energy optimal**
- + **Advantage: the battery response model can be used to accurately monitor on-line the state of charge of the battery**
- + **The methodology can be applied also to battery-powered industrial applications**



Remark

- + **The battery parameters change with time and charge/discharge cycles**
- + **They depend also on temperature. This is not taken into account in the model**

